# Synthesis of Ammonium Cyanate and Urea from NO over Pt, Os, Ru, and Cu-Ni Catalysts

R. J. H. VOORHOEVE AND L. E. TRIMBLE

Bell Laboratories, Murray Hill, New Jersey 07974
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The synthesis of NH<sub>4</sub>OCN and urea, recently reported to occur in good yields (>90%) over Pt and Rh catalysts, has been studied further over Pt, Cu-Ni, Ru, and Os catalysts. The synthesis starts from NO, which is reduced to NH<sub>4</sub>OCN with CO and H<sub>2</sub> diluted with He. Maximum yields of 98% at 360-400°C, 70% at 390°C, 28% at 250°C, and 10% at 250°C (based on 2 NO converted to NH<sub>4</sub>OCN) were obtained for Pt, Cu-Ni, Os, and Ru catalysts, respectively. The effects of temperature, flow rate, reactant concentrations, and pretreatment of the catalyst were studied for Pt catalysts. The mechanism of the formation of NH<sub>4</sub>OCN and other nitrogen products is considered. Adsorbed NCO entities appear to play a central role as intermediates.

#### INTRODUCTION

Recently, it was reported that the isomers of N<sub>2</sub>H<sub>4</sub>CO, viz., ammonium cyanate  $(NH_4OCN)$  and urea  $\lceil (NH_2)_2CO \rceil$ , were formed when NO in concentrations of 0.3 to 2% in inert gas at atmospheric pressure was reduced with CO and H2 over Pt, Rh, and Ru catalysts (1). That report also contained a review of the relevant earlier literature. Condensation of N<sub>2</sub>H<sub>4</sub>CO at low temperature (<60°C) produced NH<sub>4</sub>OCN, whereas, at higher temperatures ( $\sim 80-$ 120°C), urea was collected, apparently because of rapid conversion of the primary product NH<sub>4</sub>OCN into urea after condensation in the collector. The study of the primary process [Eq. (1)] on various catalyst surfaces,

$$2NO + 2H_2 + 3CO \rightarrow NH_4OCN + 2CO_2, \quad (1)$$

under a variety of conditions is here pursued for two reasons. First, it may yield information on the surface chemistry of the interaction of NO, CO, and H<sub>2</sub> on metals and, in particular, about the role of NCO intermediates adsorbed on the surface [see references to infrared absorption studies of NCO in Ref. (1)]. Second, the process of converting NO with CO and H<sub>2</sub> or H<sub>2</sub>O to N<sub>2</sub>H<sub>4</sub>CO at atmospheric pressure and at 300-400°C might be an economical alternative route to the two isomers, NH<sub>4</sub>OCN and (NH<sub>2</sub>)<sub>2</sub>CO. It may be noted that economical alternatives to the conventional liquid-phase high-pressure carbamate urea process are not now available (2). Although the cost of NO as a raw material is relatively high, this might in fact be overcome by the simplicity and high yield of the new process and by its ability to employ the dilute streams of NO produced by radiative processes (3), by high-temperature combustion as in the "Wisconsin process" (4), or as tail gas from the manufacture of nitric acid. Application of the new process in conjunction with HNO<sub>3</sub> manufacture might allow the latter to be

| TABLE 1                       |      |  |  |  |  |  |  |  |  |
|-------------------------------|------|--|--|--|--|--|--|--|--|
| Characterization of Catalysts | Used |  |  |  |  |  |  |  |  |

| Code      | Composition   | Preparation  | Surface<br>area <sup>a</sup><br>(m <sup>2</sup> /g) | Ref. <sup>b</sup> |
|-----------|---|--|---|-------------------|
| Pt sponge | Pt, 99.99%  | Engelhard sponge   | 0.12  | (1, 11, 12)       |
| Ru        | Ru 99.999%  | Engelhard powder   | 1.28  | (7)               |
| Cu-Ni     | Cu: Ni = 0.64:1 (at/at);<br>Cu + Ni = 97 wt% <sup>c</sup> | Fillings of commercial monel alloy   | 0.12  | (10)              |
| Os I      | Os (99.99%)   | Powder (Engelhard) in reactor reduced in H <sub>2</sub> at 100°C for 16 hr, then at 200°C for 1.4 h, and at 350°C for 45 min |   |                   |
| Os II     | Os (99,99%)   | Os I, further reduced in the<br>reactor at 450°C for 16 h in<br>90% H <sub>2</sub> in He                                     |   |                   |

<sup>&</sup>lt;sup>a</sup> Determined by N<sub>2</sub> chemisorption in a Perkin-Elmer sorption meter.

operated with much higher NO levels in the tail gas.

In the present report, the process as catalyzed by Pt, Os, Ru, and Cu-Ni is described, with emphasis on the most effective of these catalysts, Pt. It is shown that the yields of NH<sub>4</sub>OCN correspond with the published concentrations of NCO (isocyanate) surface species produced by interaction of NO and CO on supported Pt and Ru catalysts and measured by infrared absorption by Solymosi et al. (5, 6). The mechanism of the formation of N<sub>2</sub>H<sub>4</sub>CO from NO, CO, and H<sub>2</sub> is considered.

## EXPERIMENTAL METHODS

Since all experimental methods used have been described elsewhere, only a brief description will be given here. All experiments were carried out with a quartz fixed-bed reactor. The catalysts (1–5 g, Table 1) were supported on a fritted quartz disk. The reactant gases were obtained premixed in He from Scientific Gas Products, Freehold, N. J., and were blended in line with the aid of Brooks Co. flow controllers to obtain a feed-gas mixture of 0.3–2.0% NO,

0-2.0% H<sub>2</sub>, 0.4-5.0% CO, and 0-2.2% O<sub>2</sub> in He. Water was added as appropriate. The effluent from the reactor was split for on-line gas chromatographic and colorimetric analysis. Gas chromatographic analysis was used for NO,  $N_2$ , CO, and  $H_2$  (7). The conversion of NO to NH<sub>4</sub>OCN was measured continuously by quantitative absorption of NH<sub>4</sub>OCN from the effluent, conversion into urea, and colorimetric determination of urea (8) as its yellow complex with diacetyl monoxime (9). Condensed crystalline products trapped from the effluent were analyzed by ir absorption and identified as NH<sub>4</sub>OCN and (NH<sub>2</sub>)<sub>2</sub>CO (1). No quantitative analysis was done for NH<sub>3</sub>, N<sub>2</sub>O, and HCN. Earlier data on the same catalysts showed that the formation of HCN accounts for less than 1% of converted NO in the temperature range employed in the present work (10). It was also shown previously that quantitative analysis for NH<sub>3</sub> accounts for the balance of the N derived from NO at temperatures above 400°C (10, 11). Deficits in the N balance below about 350°C are assumed to be due to formation of  $N_2O$ .

<sup>&</sup>lt;sup>b</sup> References to earlier work in this laboratory on the same catalyst.

<sup>&</sup>lt;sup>c</sup> Analysis by Fairfield Testing Labs, Fairfield, N.J.

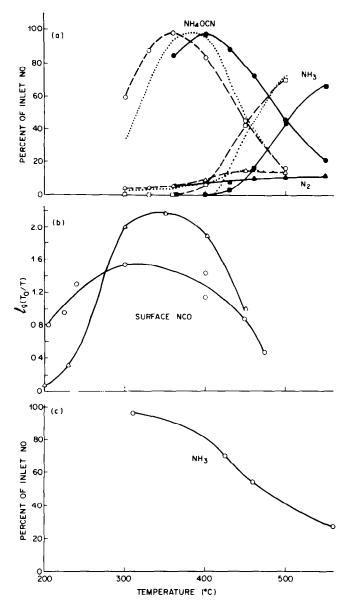


Fig. 1. Conversion of NO over Pt sponge. (a) Percentage of N in inlet NO recovered as NH<sub>4</sub>OCN, NH<sub>3</sub>, and N<sub>2</sub> is plotted. Prereduced catalyst. Flow rates, normalized per square meter of Pt in the sample, are  $1.15 \times 10^4$  (--- and symbols),  $2.3 \times 10^4$  [..., from ref. (1)], and  $4.0 \times 10^4$  (-- and filled symbols) ml/h/m². Standard concentrations of NO (0.3%), H<sub>2</sub> (0.5%), and CO (5%). (b) Isocyanate groups on the surface of 5% Pt/Al<sub>2</sub>O<sub>3</sub> measured by ir absorption at 2267 cm<sup>-1</sup>: ( $\bigcirc$ ) reduced sample; ( $\triangle$ ) oxidized sample, after Solymosi et al. ( $\delta$ ); (c) NH<sub>3</sub> formed in the reduction of 0.1% NO with 1.4% H<sub>2</sub> and 1.5% CO over a Pt/Al<sub>2</sub>O<sub>3</sub> catalyst, after Shelef and Gandhi (1 $\theta$ ).

### RESULTS

### **Platinum**

The formation of NH<sub>4</sub>OCN, NH<sub>3</sub>, and N<sub>2</sub> from a "standard mixture" (0.3% NO,

0.5% H<sub>2</sub>, and 5% CO in He) over a Pt sponge catalyst is given in Fig. 1 as a function of the temperature of the catalyst. Three values of the flow rate were used, viz.,  $1.15 \times 10^4$ ,  $2.3 \times 10^4$ , and  $4.0 \times 10^4$ 

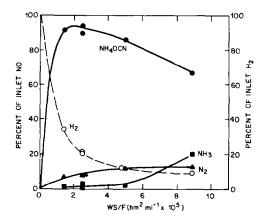


Fig. 2. Conversion of NO over Pt sponge at 430°C. Catalyst as in Fig. 1. Flow rates normalized per square meter of Pt in the sample. Standard gas mixture.

ml/h/m<sup>2</sup> of Pt in the sample, respectively. This corresponds to GHSV values of 6800 to 23,500 h<sup>-1</sup>. The data for  $2.3 \times 10^4$  ml/ h/m<sup>2</sup> are from Ref. (1). Prior to use, the catalysts were reduced in 2% H2 in He at 475-500°C for 11 h or longer. Without prereduction, the results are similar to those in Fig. 1, except that the yields of N<sub>2</sub> are somewhat higher and the yields of NH<sub>4</sub>OCN are correspondingly lower. The effect of increasing flow rate is primarily to shift the yield curves, including the optimum yield of NH<sub>4</sub>OCN, to higher temperature. This optimum, which is close to 100%, is in all cases reached at the temperature at which NO is just completely

converted (NO is not shown for clarity). Figure 2 shows the effect of reciprocal flow rate on the conversion of NO into N<sub>2</sub>, NH<sub>3</sub>, and NII<sub>4</sub>OCN over the same catalyst (Pt sponge) at 430°C. NH<sub>4</sub>OCN appears to be a primary product, followed by formation of NH<sub>3</sub>.

The composition of the feed gas has been varied to study the effects on the yield of NH4OCN. At constant levels of NO and H2 (0.3% each), the concentration of CO has been varied from 0.4-5.0%. Figure 3 shows the results of two series of experiments: one with a freshly reduced Pt sponge and the other with the same Pt sponge after it had been stored under He for 4 days without regeneration and apparently had lost some of its selectivity. The temperature for both series was 404°C, and the flow rate was  $4.0 \times 10^4$  ml/h/m<sup>2</sup>. The variations of the yield with the concentration of CO are similar in both series; a substantial drop in selectivity occurs only below 2% CO. For the reaction of Eq. (1), this corresponds to a fourfold excess of CO. For the less selective, used catalyst, the effect of increasing the concentrations of NO and H<sub>2</sub> (at  $NO/H_2 = 1.0$ ) at a constant CO concentration (5%) is given in Fig. 4. A significant decline in selectivity occurs here when the amount of CO is less than 2.5 times the stoichiometric amount.

Industrial streams containing NO often

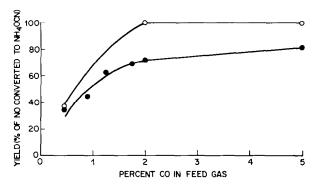


Fig. 3. Effect of CO concentration on the yield of NH<sub>4</sub>OCN over Pt sponge at 404°C. Flow rate:  $4.0 \times 10^4$  ml/h/m². Concentrations of NO and H<sub>2</sub> are 0.3%. Open symbols: freshly reduced Pt; filled symbols: same catalyst after extended use without regeneration.

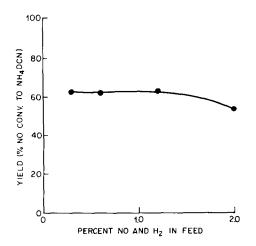


Fig. 4. Effect of NO and H<sub>2</sub> concentrations on the yield of NH<sub>4</sub>OCN over Pt sponge at 420°C. Flow rate: 4.0×10<sup>4</sup> ml/h/m². Concentration of CO: 5℃. Used catalyst as in Fig. 3.

contain  $O_2$  and  $H_2O$ . Figure 5 shows the effect of adding  $O_2$  to the standard gas mixture, maintaining NO,  $H_2$ , and CO at 0.3, 0.5, and 5%, respectively. The catalyst is the Pt sponge and the flow rate is  $2.3 \times 10^4$  ml/h/m². Series of experiments at 409 and 500°C are shown. At 409°C, a deleterious effect of  $O_2$  on the yield of NH<sub>3</sub>OCN is noted only beyond 2.2%  $O_2$ , i.e., when the amount of  $O_2$  is close to the stoichiometric amount necessary for Eq. (1) plus oxidation of CO. At 500°C, small amounts of  $O_2$  in the feed gas enhance the yield of NH<sub>4</sub>OCN at the expense of NH<sub>3</sub>.

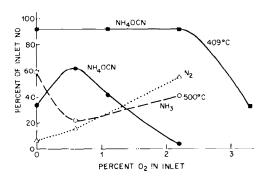


Fig. 5. Effect of  $O_2$  on the conversion of NO over Pt sponge at 409 and 500°C. Prereduced catalyst, Flow rate:  $2.3 \times 10^4 \text{ ml/h/m}^2$ . Standard concentrations of NO (0.3%),  $H_2$  (0.5%), and CO (5.0%).

TABLE 2
Formation of NH<sub>4</sub>OCN from NH<sub>3</sub> over Pt Sponge<sup>a</sup>

| Experiment No. | Gas composition ( $C_o$ in He) |      |                 | <i>T</i><br>(°C) | Conversion of |  |
|----------------|--------------------------------|------|-----------------|------------------|---------------|--|
|                | NH <sub>3</sub>                | СО   | CO <sub>2</sub> | $O_2$            |               | NH <sub>3</sub> to<br>NH <sub>4</sub> OCN<br>(%) |
| 1              | 1.33                           | 0.67 |                 |                  | 450           | 1.6  |
| $^2$           | 1.33                           | 0.67 |                 | 0.05             | 450           | 2.0  |
| 3              | 0.3                            | 1.7  |                 |                  | 450           | 3.2  |
| 4              | 1.33                           |      | 0.67            |                  | 450           | 0  |
| 5              | 0.3                            |      | 1.7             | 0.15             | 380           | 0.3  |
| 6              | 0.3                            |      | 1.7             | 0.3              | 380           | 0.7  |

<sup>&</sup>lt;sup>a</sup> Flow rate:  $1.15 \times 10^4$  ml/h/m<sup>2</sup>,

Beyond the addition of 1.2% O<sub>2</sub>, the yield of NH<sub>4</sub>OCN is diminished with respect to the O<sub>2</sub>-free reaction mixture. The effect of water on the yield of NH<sub>4</sub>OCN has been reported previously (1). Water could be used instead of H<sub>2</sub> to supply H for N<sub>2</sub>H<sub>4</sub>CO in the temperature range near 400°C (1). At lower temperatures, near those where NO is first completely converted, hydrolysis of cyanate to NH<sub>3</sub> was observed to occur at relatively high rates (13).

Since there have been reports (14, 15) that NH<sub>3</sub> may react with CO or CO<sub>2</sub> according to

$$CO + 2NH_3 \rightarrow N_2H_4CO + H_2 \qquad (2)$$

and

$$CO_2 + 2NH_3 \rightarrow N_2H_4CO + H_2O$$
, (3)

we have attempted these reactions over the fresh, prereduced Pt sponge catalyst to ascertain whether NH<sub>3</sub> formed in the reduction of NO could be an intermediate in the formation of the cyanate group. With gas mixtures containing NH<sub>3</sub> (0.3–1.3%), CO (0.6–1.7%), and O<sub>2</sub> (0–0.05%) in He or NH<sub>3</sub> (0.3–1.3%), CO<sub>2</sub> (0.6–1.7%), and O<sub>2</sub> (0.15–0.3%) in He, at a flow rate of 1.15  $\times$  10<sup>4</sup> ml/h/m² and in the temperature range of 250–550°C, a maximum yield of NH<sub>4</sub>OCN (calculated on NH<sub>3</sub> inlet) of 3% was obtained. The "best" yields were obtained with a mixture of 0.3% NH<sub>3</sub> and

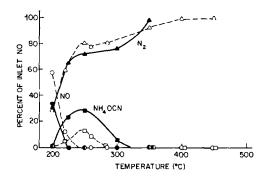


Fig. 6. Conversion of NO over Os catalyst. Percentage of N in inlet NO recovered as NO, N<sub>2</sub>, and NH<sub>4</sub>OCN is plotted. Flow rate:  $4.6\times10^3$  ml/h/m<sup>2</sup> of Os in the sample. Standard concentrations of NO (0.3%), H<sub>2</sub> (0.5%), and CO (5.0%) in He. Heavy lines and filled symbols: Os I catalyst. Light lines and open symbols: Os II catalyst.

1.7% CO. Small additions of O<sub>2</sub> increased the yield (Table 2).

# Osmium and Ruthenium

A very gradual prereduction of the Os metal powder was used to prevent the evolution of highly volatile  $OsO_4$  (Table 1). The results in the reduction of NO were found to be susceptible to the oxidation state of the catalyst to a stronger degree than was the case for Pt. Figure 6 shows that  $N_2$  is the predominant product of the reduction. The standard mixture of NO,  $H_2$ , and CO in He was used at a rate of flow of  $4.6 \times 10^3$  ml/h/m². A moderate prereduction of the catalyst gave a higher yield of  $NH_4OCN$  (28% at 250°C) than a more thorough prereduction procedure (which yielded 13% at 250°C).

A study of the reduction of NO with CO and  $\rm H_2$  over Ru was published before (7). The yield of NH<sub>3</sub> showed two peaks, centered at approximately 250 and 380°C. The same catalyst was used in the present experiments. Figure 7a shows the yield of NH<sub>4</sub>OCN, with a maximum near 240°C, observed with the standard mixture of gases used at a flow rate of  $1.2 \times 10^4$  ml/h/m². The peak value of 10.5% decreased to 6% when the flow rate was cut in half.

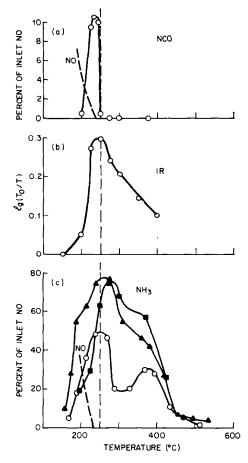


Fig. 7. Ru in the interaction of NO, CO, and H<sub>2</sub>. (a) Present work. Percentage of N in inlet NO recovered as NH4OCN and NO versus catalyst temperature. Prereduced unsupported catalyst. Standard gas mixture of NO (0.3%), H<sub>2</sub> (0.5%), and CO (5%) in He at a flow rate of  $1.2 \times 10^4$ ml/h/m², corresponding to a GHSV of 90,000 h<sup>-1</sup>. (b) Concentration of NCO surface species on a reduced 5% Ru/Al<sub>2</sub>O<sub>3</sub> catalyst after 30 min of contact with 100 Torr of a mixture of 5% NO, 10% CO, and 85% N<sub>2</sub> at the temperature indicated. Measured by ir absorption (2265 cm<sup>-1</sup>) at room temperature by Solymosi and Rasko (6). (c) Yield of NH3 in the reduction of NO with H2 and CO (O) Data on unsupported Ru sponge, with mixture W of NO (0.13%), H<sub>2</sub> (0.4%), CO (1.3%), H<sub>2</sub>O (3%), and  $CO_2$  (3%) in He at GHSV=33,000 h<sup>-1</sup>, after Voorhoeve and Trimble (?); (▲) data on a reduced 0.8% Ru/Al<sub>2</sub>O<sub>3</sub> catalyst with the same mixture W at  $GHSV = 18,000 \text{ h}^{-1}$  (7); ( $\blacksquare$ ) data on a 0.5% Ru/Al<sub>2</sub>O<sub>3</sub> catalyst with a mixture of NO (0.1%),  $H_2$  (1.4%), and CO (1.5%) in  $N_2$  at GHSV = 20,000 h<sup>-1</sup>, after Shelef and Gandhi (16).

Monel (Cu Ni)

The eatalyst was prereduced in flowing pure  $H_2$  at  $450^{\circ}$ C. Figure 8 shows the conversion of NO into  $N_2$  and  $NH_4OCN$  in dependence of the temperature of the catalyst. The standard gas mixture was used at a flow rate of  $1.6 \times 10^4$  ml, h/m². The maximum yield of  $NH_4OCN$  was 70%. In an interval of  $10^{\circ}$ C this decreases to 0%. This behavior was reproducible, and the steep section of the yield–temperature curve could be traversed in both reactions with no hysteresis. There was no corresponding feature in the yield of  $N_2$ .

#### DISCUSSION

In the data collected for Pt, it is striking that a very high yield of NH<sub>4</sub>OCN was obtained over a wide range of operating conditions (Figs. 1–3). It is particularly evident that NH<sub>4</sub>OCN and N<sub>2</sub> are the only products over an appreciable range of low-temperature ( $\lesssim 400^{\circ}$ C) conditions. No isocyanic acid (HNCO) was detected. This strongly suggests that NCO intermediates on the surface can only desorb as NH<sub>4</sub>OCN, i.e., that a step like

$$NCO + NH_4^+ \rightarrow NH_4OCN$$
 (4a)

or

$$HNCO(ads) + NH_3 \rightarrow NH_4OCN$$
, (4b)

due to the lack of NH<sub>3</sub>, is the rate-determining step in the conversion of NO to cyanate in the gas phase. It has indeed been found that the addition of NH<sub>3</sub> to the feed strongly enhances the conversion of NO to cyanate over a Pt-10% Rh catalyst (13). At temperatures of 400°C and below, surface NCO groups are rather stable on Pt in the presence of NO and CO. The amount of NCO found by ir absorption after contacting (at temperature T) a Pt/Al<sub>2</sub>O<sub>3</sub> catalyst with NO/CO mixtures with an excess of CO shows a dependence on T which is rather strikingly similar to the temperature profile of NH<sub>4</sub>OCN forma-

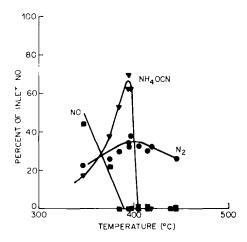


Fig. 8. Conversion of NO over a Cu-Ni (monel) catalyst. Percentage of N in inlet NO recovered as NO, N<sub>2</sub>, and NH<sub>4</sub>OCN. Prereduced unsupported catalyst. Standard gas mixture at a flow rate of 1.6×10<sup>4</sup> ml/hr/m<sup>2</sup>.

tion in Fig. 1, except that the NCO peak measured by ir extends to lower temperature (5). Removal of NCO from the surface is, at low temperature ( $\lesssim 400$ °C), proposed to be limited by the prerequisite hydrolysis of NCO to form NH<sub>3</sub>, a reaction first proposed by Unland (17, 18):

$$NCO^{-} + 2 H_{2}O \rightarrow NH_{3} + OH^{-} + CO_{2}.$$
 (5)

On oxidic surfaces such as provided by the oxide support [to which NCO groups may migrate (19)], Eq. (5) may reasonably be expected to dominate over Eq. (4a) or (4b), in agreement with the experience (1) that NH<sub>3</sub> rather than NH<sub>4</sub>OCN is the main product for the reduction of NO with CO and  $H_2$  (or  $H_2O$ ) over  $Pt/Al_2O_3$  catalysts. At low temperature, NCO is relatively unreactive to H<sub>2</sub>, on both Pt/Al<sub>2</sub>O<sub>3</sub> and  $Pd/Al_2O_3$  (18, 20) suggesting again that hydrolysis, rather than hydrogenation, is the preferred route to NH<sub>3</sub> at  $T \lesssim 400$ °C. The hydrolysis is slow on unsupported Pt, however, and high yields of NH<sub>4</sub>OCN were obtained even in the presence of 5% H<sub>2</sub>O at 400°C (1). However, at higher temperatures hydrogenation of the NCO or NH<sub>4</sub>OCN species is possible, as shown by the increase of NH<sub>3</sub> formation at the expense of NH<sub>4</sub>OCN when the concentration of H<sub>2</sub> is increased (1, 13). A consecutive reaction,

$$NH_4OCN + H_2 \rightarrow 2 NH_3 + CO$$
, (6)

is in agreement with the data for 430°C in Fig. 2 which show that NH<sub>4</sub>OCN is a primary product, whereas free NH<sub>3</sub> is only formed at much longer residence times. Finally, the data in Fig. 5 show that preferential removal of H2 with O2 increases the yield of NH<sub>4</sub>OCN and decreases the yield of NH<sub>3</sub> at 500°C, in agreement with the reaction scheme of Eqs. (4)-(6). Comparison of Fig. 1c with Figs. 1a and b suggests that the formation of NH<sub>3</sub> on Pt/Al<sub>2</sub>O<sub>3</sub> may very well be accounted for by hydrolysis and hydrogenation of cyanate intermediates. Naturally, such a cross correlation of data from different sources cannot be definitive.

The mechanisms of the formation of NH<sub>4</sub>OCN and NH<sub>3</sub> over Rh (1), Cu-Ni, Ru, and Os are expected to be similar, but, of course, the relative yields of the various products will be different due to different oxidation states of the surfaces and different relative rates of the various processes. Isocyanate or cyanate surface species have been reported in studies of the interaction of CO and NO with Ru/Al<sub>2</sub>O<sub>3</sub> (6, 17) and CuO/SiO<sub>2</sub> (21), as well as with Rh/Al<sub>2</sub>O<sub>3</sub> (17, 22).

Figure 7 shows that (for Ru) the three phenomena (NH<sub>4</sub>OCN formation, detection of NCO at the surface by ir, and production of NH<sub>3</sub> by reduction of NO) appear to be related in a similar way as in the case of Pt. It should be noted that the formation of NH<sub>3</sub> over Ru catalysts was reported to be promoted by CO in the range of the low-temperature peaks in Fig. 7c (7, 16, 23), whereas the high-temperature NH<sub>3</sub> peak was promoted by H<sub>2</sub> (7). The correlation extends to the relative stability of NCO and the yield of NH<sub>4</sub>OCN:

Stability (6) and yield are much lower for Ru than for Pt catalysts. Finally, it is noted that the rates of formation of NH<sub>4</sub>OCN and of NH<sub>3</sub> are comparable in the temperature range in which the cyanate is proposed to be an intermediate for the formation of NH<sub>3</sub> (200-300°C). There is no evidence for cyanate as an intermediate or product over Ru at higher temperatures.

# CONCLUSIONS

Reduction of NO with CO and H2 over unsupported Pt catalysts is an efficient, highyield process for the formation of ammonium cyanate and urea. Yields of 95% have been obtained at temperatures of 400°C and below, with complete conversion of NO. There is mounting evidence for the important role of (iso)cyanate surface species as crucial intermediates in the formation of NH<sub>4</sub>OCN and NH<sub>3</sub>. The reactions of the NCO intermediate are likely to include hydrolysis to NII<sub>3</sub>, desorption as NH<sub>4</sub>OCN after reaction with NH<sub>3</sub>, and hydrogenation to NH<sub>3</sub>. At low temperature (<400°C), desorption and hydrolysis dominate, whereas, at higher temperature (>400°C), hydrogenation becomes important.

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